

### Solution 1

Given : volume of ice cream pack ( $V$ ) =  $0.2 \times 0.1 \times 0.07 \text{ m}^3$   
 $= 1.4 \times 10^{-3} \text{ m}^3$

Initial temperature of ice cream ( $T_0$ ) =  $-10^\circ\text{C}$

Time ( $t$ ) = 20 minutes  
 $= 1200 \text{ seconds}$

Ice cream properties →

$$K = 2.2 \text{ W/m}^\circ\text{C}$$

$$C = 1800 \text{ J/kg}^\circ\text{C}$$

$$\rho = 900 \text{ kg/m}^3$$

$$h = 10 \text{ W/m}^2 \text{ }^\circ\text{C}$$

### Assumptions

- i) Internal energy and the temperature of the ice-cream decreases as a result of transient heat conduction.
- ii) Assuming atmospheric temperature ( $T_\infty$ ) as  $25^\circ\text{C}$

### Analysis

The Biot number ( $Bi$ ) is determined from

$$Bi = \frac{h L_c}{K}$$

Here  $L_c$  = characteristic length of the ice cream pack

$$= \frac{\text{Volume}}{\text{Surface area}}$$

$$= \frac{1.4 \times 10^{-3}}{2[(0.2)(0.1) + (0.1)(0.07) + (0.07)(0.2)]}$$

$$\Rightarrow L_c = 0.017 \text{ m}$$

$$\Rightarrow Bi = \frac{hL_c}{k} = \frac{10 \times 0.017}{2.2}$$

$$= 0.077$$

Since Biot number is less than 0.1  
therefore, lumped analysis is valid

$\Rightarrow$  we can assume the whole ice-cream pack at uniform temperature and write the following relation using energy conservation equation

i.e.  $\frac{T - T_{\infty}}{T_i - T_{\infty}} = e^{-\left(\frac{hA_s}{\rho V C_p}\right)t}$

Here,  $T_i$  = initial temperature of ice-cream pack =  $-10^{\circ}\text{C}$

$T$  = final temperature of ice-cream pack

$T_{\infty}$  = surrounding temperature =  $25^{\circ}\text{C}$

$A_s$  = surface area of ice cream pack

$V$  =  $L_c$  = characteristic length =  $0.017\text{ m}$

$C_p$  = Heat capacity of ice cream =

Putting given values in above relation  $\rightarrow$

$$\frac{T - 25}{-10 - 25} = e^{-\left(\frac{10 \times 1200}{900 \times 0.017 \times 1800}\right)t}$$

$$\Rightarrow \frac{T - 25}{-35} = e^{-0.435t}$$

$$\Rightarrow T - 25 = (-35)(0.647) = -22.6^{\circ}\text{C}$$

$$\Rightarrow \boxed{T = 2.36^{\circ}\text{C}}$$

Since, the final temperature of the ice cream (i.e.  $2.36^{\circ}\text{C}$ ) is above  $0^{\circ}\text{C}$ , it will melt.

And the kids will not eat the ice-cream

### Solution 2

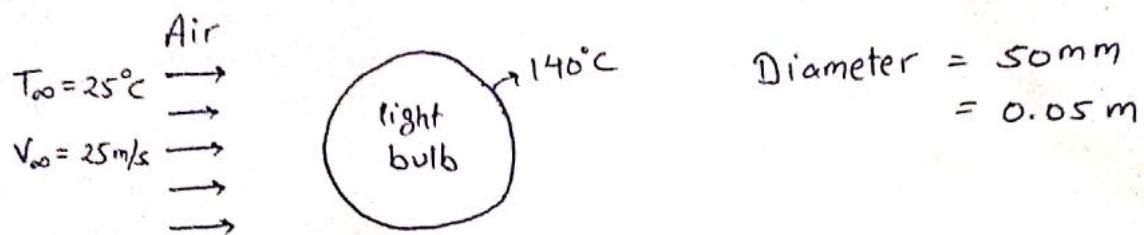


Fig: Schematic of the problem

### Assumptions

- steady operating conditions exist
- Radiation effects are negligible
- Air behaves like an ideal gas
- The outer surface temperature of the light bulb is uniform at all times.
- The surface temperature of the light bulb is kept constant.

### Properties

The dynamic viscosity of air at the surface temperature is

$$\mu_s = \mu_{140^{\circ}\text{C}} = 2.345 \times 10^{-5} \text{ kg/m-s.}$$

The properties of air at the free stream temperature of  $25^{\circ}\text{C}$  and atmospheric pressure are obtained from (table A-15)

$$K = 0.02551 \text{ W/m}^{\circ}\text{C}$$

$$\nu = 1.562 \times 10^{-5} \text{ m}^2/\text{s}$$

$$\mu = 1.849 \times 10^{-5} \text{ kg/m.s}$$

$$\rho_r = 0.7296$$

Reynolds number is determined from

$$Re = \frac{V D}{\nu}$$

$$= \frac{(25 \text{ m/s})(0.05 \text{ m})}{1.562 \times 10^{-5} \text{ m}^2/\text{s}}$$

$$= \underline{\underline{8 \times 10^4}}$$

The Nusselt number is determined from Whitaker correlation for flow over a sphere →

$$Nu = \frac{h D}{K} = 2 + \left[ 0.4 Re^{1/2} + 0.06 Re^{2/3} \right] Pr^{0.4} \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4}$$

$$= 2 + \left[ 0.4 (8 \times 10^4)^{1/2} + 0.06 (8 \times 10^4)^{2/3} \right] (0.7296)^{0.4} \times \left( \frac{1.849 \times 10^{-5}}{2.345 \times 10^{-5}} \right)^{1/4}$$

$$= 2 + [113.155 + 111.422] (0.881) (0.893)$$

$$= \underline{\underline{178.64}}$$

⇒ the average convection heat transfer coefficient becomes

$$h = \frac{K}{D} Nu$$

$$= \frac{0.02551 \text{ W/m}^\circ\text{C}}{0.05 \text{ m}} \times 178.64$$

$$= \underline{\underline{91.145 \text{ W/m}^2 \circ\text{C}}}$$

$\Rightarrow$  Heat transfer rate from the light bulb to the surrounding is given by  $\rightarrow$

$$\dot{Q} = h A_s (T_s - T_{\infty})$$

Here  $A_s$  = surface area =  $4\pi r^2$

$T_s$  = surface temperature of light bulb =  $140^\circ\text{C}$

$T_{\infty}$  = surrounding air temperature =  $25^\circ\text{C}$

$$\Rightarrow \dot{Q} = (91.145 \text{ W/m}^2\text{ }^\circ\text{C}) (4\pi (0.05)^2) \text{ m}^2 (140 - 25)^\circ\text{C}$$

$$= (91.145) (7.857 \times 10^{-3}) (115) \text{ W}$$

$$= \boxed{82.35 \text{ W}}$$

### Solution 3

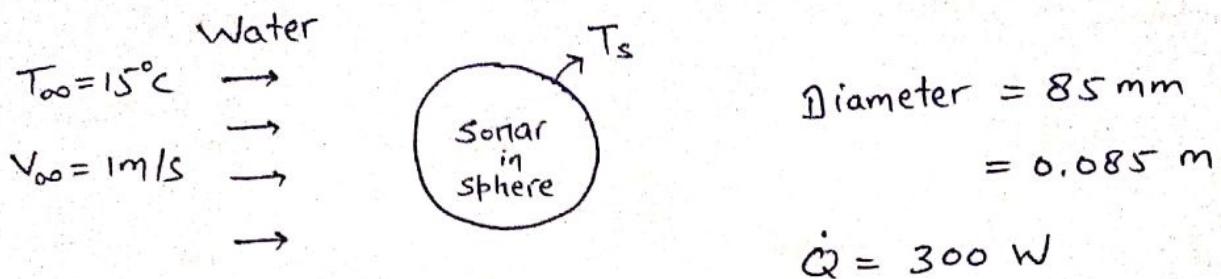


Fig: Schematic of the problem

### Assumptions

- i) steady operating conditions exist
- ii) Radiation effects are negligible
- iii) Air behaves like an ideal gas
- iv) The outer surface of the sphere has uniform temperature.

### Properties of water

The dynamic viscosity of water at the surface temperature

$$\text{is } \mu_s = \mu @ T_s$$

The properties of water at the free stream temperature of  $15^{\circ}\text{C}$  are as follows

$$K = 0.588 \text{ W/mK}$$

$$\gamma = 1.15 \times 10^{-6} \text{ m}^2/\text{s}$$

$$\mu = 1.15 \times 10^{-3} \text{ Ns/m}^2$$

$$\Pr = 8.23$$

Reynolds number is given by

$$\begin{aligned} Re &= \frac{V D}{\nu} \\ &= \frac{(1 \text{ m/s})(0.085 \text{ m})}{1.15 \times 10^{-6} \text{ m}^2/\text{s}} \\ &= \underline{\underline{73913}} \end{aligned}$$

Nusselt number is given by

$$\begin{aligned} Nu &= \frac{h D}{K} = 2 + \left[ 0.4 Re^{1/2} + 0.06 Re^{2/3} \right] \left[ Pr^{0.4} \right] \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \\ &= 2 + \left[ 0.4 (73913)^{1/2} + (0.06) (73913)^{2/3} \right] (8.23)^{0.4} \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \\ &= 2 + (108.74 + 105.67)(2.32) \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \\ &= 2 + 498.22 \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \quad \textcircled{1} \end{aligned}$$

Now, Dynamic viscosity of water at various temperatures  $\rightarrow$

$$\mu_{\infty} = \mu_{15^\circ\text{C}} = 1.15 \times 10^{-3}$$

$$\mu_{20^\circ\text{C}} = 1.002 \times 10^{-3}$$

$\Rightarrow$  by interpolation

$$\mu_T = (1.612 - 0.0305 T) \times 10^{-3}$$

$\Rightarrow$  Putting in equation ①

$$Nu = 2 + 498.22 \left( \frac{1.15 \times 10^{-3}}{(1.612 - 0.0305 T_s) \times 10^{-3}} \right)^{1/4}$$

$$\Rightarrow N_u = 2 + 498.22 \times \left( \frac{1.15}{1.612 - 0.0305 T_s} \right)^{1/4}$$

$\Rightarrow$  average convection heat transfer coefficient is given by  $\rightarrow$

$$h = \frac{K}{D} N_u$$

$$= \left( \frac{0.588}{0.085} \right) \left[ 2 + 498.22 \times \left( \frac{1.15}{1.612 - 0.0305 T_s} \right)^{1/4} \right]$$

$$= 13.835 + 3446.51 \times \left( \frac{1.15}{1.612 - 0.0305 T_s} \right)^{1/4}$$

given Heat transfer rate  $\dot{Q} = 300W$

$$\Rightarrow \dot{Q} = 300W = h A_s (T_s - T_\infty)$$

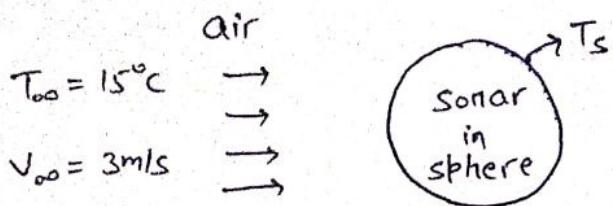
$$\Rightarrow 300 = \left[ 13.835 + 3446.51 \times \left( \frac{1.15}{1.612 - 0.0305 T_s} \right)^{1/4} \right] \left( 4\pi \left( \frac{0.085}{2} \right)^2 \right) \times (T_s - 15)$$

$$\Rightarrow 2 \times 6605.85 = (T_s - 15) \left[ 13.835 + 3446.51 \times \left( \frac{1.15}{1.612 - 0.0305 T_s} \right)^{1/4} \right]$$

By solving above equation, we get

$$T_s = 18.89^\circ C \quad \text{sonar surface temperature}$$

Now, when the sonar was put into air →



Properties of air at free stream temperature of  $15^{\circ}\text{C}$  →

$$K = 0.02476 \text{ W/mK}$$

$$\nu = 1.470 \times 10^{-5} \text{ m}^2/\text{s}$$

$$\Pr = 0.7323$$

$$\mu = 1.8 \times 10^{-5} \text{ Ns/m}^2$$

Reynolds number is given by →

$$Re = \frac{V D}{\nu}$$

$$= \frac{(3 \text{ m/s})(0.085 \text{ m})}{1.470 \times 10^{-5} \text{ m}^2/\text{s}}$$

$$= \underline{\underline{17347}}$$

Nusselt number is given by

$$Nu = \frac{h D}{K} = 2 + \left[ 0.4 Re^{1/2} + 0.06 Re^{2/3} \right] (\Pr^{0.4}) \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4}$$

$$= 2 + \left[ 0.4 (17347)^{1/2} + 0.06 (17347)^{2/3} \right] (0.7323)^{0.4} \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4}$$

$$= 2 + 82 \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \quad \textcircled{2}$$

Now, dynamic viscosity of air at various temperatures  $\rightarrow$

$$\mu_{\infty} = \mu_{15^{\circ}\text{C}} = 1.8 \times 10^{-5}$$

$$\mu_{20^{\circ}\text{C}} = 1.825 \times 10^{-5}$$

$\Rightarrow$  by interpolation

$$\mu_T = (1.731 + 0.0047T) \times 10^{-5}$$

Putting in equation ②

$$Nu = \frac{hD}{k} = 2 + 82 \times \left( \frac{1.8}{1.731 + 0.0047T} \right)^{1/4}$$

$$\begin{aligned} \Rightarrow h = \frac{k}{D} Nu &= \frac{0.02476}{0.085} \times \left[ 2 + 82 \times \left( \frac{1.8}{1.731 + 0.0047T} \right)^{1/4} \right] \\ &= 0.582 + 23.89 \left( \frac{1.8}{1.731 + 0.0047T} \right)^{1/4} \end{aligned}$$

given, Heat transfer rate  $\dot{Q} = 300 \text{ W}$

$$\Rightarrow \dot{Q} = 300 \text{ W} = h A_s (T_s - T_{\infty})$$

$$\Rightarrow 300 = \left[ 0.582 + 23.89 \left( \frac{1.8}{1.731 + 0.0047T_s} \right)^{1/4} \right] \left( 4\pi \left( \frac{0.085}{2} \right)^2 \right) (T_s - 15)$$

$$\Rightarrow 13211.7 = (T_s - 15) \left[ 0.582 + 23.89 \left( \frac{1.8}{1.731 + 0.0047T_s} \right)^{1/4} \right]$$

By solving above equation, we get

$$T_s = 709.34^{\circ}\text{C} \quad \text{soil surface temperature}$$

Since, the surface temperature of sphere (i.e.  $709.34^{\circ}\text{C}$ ) in air is very high, this is a reason of concern. It may result in temperature stress on sphere material.

## Solution 4

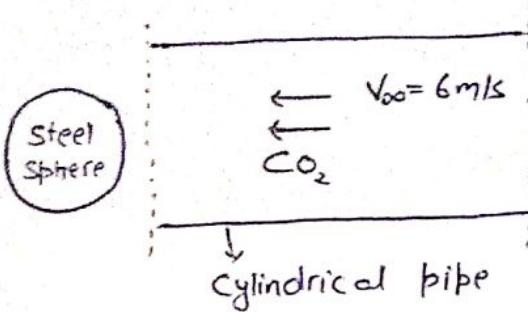


Fig: schematic of the problem

given, diameter of sphere =  $d = 5 \text{ cm}$

diameter of pipe =  $D = 10 \text{ cm}$

Pipe temperature at entrance =  $350 \text{ K}$

Pipe temperature at exit =  $550 \text{ K}$

$$\Rightarrow \text{Average temperature of pipe} = \frac{350 \text{ K} + 550 \text{ K}}{2}$$
$$= 450 \text{ K}$$

gas temperature at entrance =  $300 \text{ K}$

gas temperature at exit =  $340 \text{ K}$

$$\Rightarrow \text{Average temperature of gas} = \frac{300 \text{ K} + 340 \text{ K}}{2}$$
$$= 320 \text{ K}$$

### Assumptions

i) Steady operating conditions exist

ii) Radiation effects are negligible

iii)  $\text{CO}_2$  behaves like an ideal gas

Properties of  $\text{CO}_2$  at average temperature (i.e. at 320 K) →

$$K = 0.0396 \text{ W/mK}$$

$$C_p = 1070 \text{ J/kgK}$$

$$\mu = 2.758 \times 10^{-5} \text{ kg/m.s}$$

$$\nu = 3.061 \times 10^{-5} \text{ m}^2/\text{s}$$

$$\Pr = 0.7452$$

$$\rho = 0.9636 \text{ kg/m}^3$$

Reynolds number for the flow of  $\text{CO}_2$  in the pipe

is given by →

$$Re = \frac{V D}{\nu}$$

$$= \frac{(6 \text{ m/s})(0.1 \text{ m})}{3.061 \times 10^{-5} \text{ m}^2/\text{s}}$$

$$= \underline{\underline{19601}}$$

Nusselt number for flow through cylindrical pipe is

given by →

$$Nu = \frac{hD}{K} = 0.193 Re^{0.618} Pr^{1/3} \quad [\text{for } 4,000 < Re < 40,000]$$

$$= (0.193)(19601)^{0.618} (0.7452)^{1/3}$$

$$= (0.193)(449.4)(0.9066)$$

$$= \underline{\underline{78.63}}$$

⇒ convective heat transfer coefficient of the gas moving

$$\text{in the pipe } (h) = \frac{K}{D} Nu$$

$$= \frac{0.0396}{0.1} \times 78.63 = \boxed{31.14 \text{ W/m}^2\text{K}}$$

Now, let the length of the pipe = L

then, by principle of energy conservation →  
Energy gained by the gas = Energy supplied by the pipe  
via convection

$$\Rightarrow \dot{m} c_p \Delta T_{\text{gas}} = h A_s \Delta T_{\text{avg}}$$

Here  $\dot{m}$  = mass flow rate of the gas

$$= \rho A_{c,s} V_\infty$$

$$= (0.9636) \left( \frac{\pi D^2}{4} \right) (6)$$

$$\Rightarrow (0.9636) \left( \frac{\pi D^2}{4} \right) (6) (1070) \Delta T_{\text{gas}} = h (\pi D L) \Delta T_{\text{avg}}$$

$$\Rightarrow 154.66 \Delta T_{\text{gas}} = h L \Delta T_{\text{avg}}$$

$\Delta T_{\text{gas}}$  = increase in temperature of gas

$$= 340 \text{ K} - 300 \text{ K}$$

$$= 40 \text{ K}$$

$\Delta T_{\text{avg}}$  = average temperature difference between the pipe and the gas

$$= 450 \text{ K} - 320 \text{ K}$$

$$= 130 \text{ K}$$

$$\Rightarrow 154.66 \Delta T_{\text{gas}} = h L \Delta T_{\text{avg}}$$

$$\Rightarrow 154.66 \times 40 = (31.14)(L)(130)$$

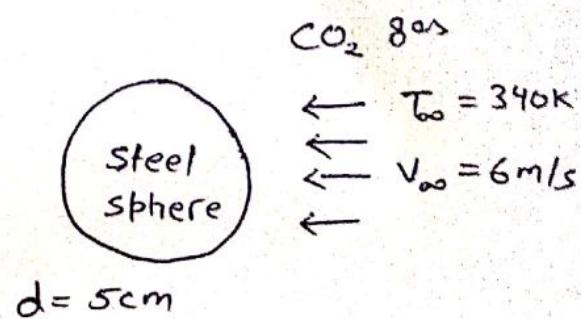
$$\Rightarrow \boxed{L = 1.53 \text{ m}} \quad \text{Length of pipe}$$

Now, heat transfer rate at the pipe is given by

$$\begin{aligned}\dot{Q} &= h A_s (\Delta T)_{avg} \\ &= h (\pi D L) \Delta T_{avg} \\ &= (31.14 \text{ W/m}^2\text{K}) (\pi \times 0.1 \times 1.53 \text{ m}^2) (130 \text{ K}) \\ &= \boxed{1944.3 \text{ W}}\end{aligned}$$

Now, interaction between gas and sphere

$$\begin{aligned}Re &= \frac{\nu d}{\eta} \\ &= \frac{(6 \text{ m/s})(0.05)}{3.2564 \times 10^{-5}} \\ &= \underline{\underline{9213}}\end{aligned}$$



Properties of gas at 340K

$$k = 0.0411 \text{ W/mK}$$

$$\mu = 2.833 \times 10^{-5}$$

$$\nu = 3.2564 \times 10^{-5}$$

$$\Pr = 0.7453$$

Nusselt number is given by Whitaker correlation

$$\begin{aligned}\text{i.e. } Nu &= \frac{h D}{k} = 2 + \left[ 0.4 Re^{1/2} + 0.06 Re^{2/3} \right] (\Pr^{0.4}) \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \\ &= 2 + \left[ 0.4 (9213)^{1/2} + 0.06 (9213)^{2/3} \right] (0.7453)^{0.4} \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \\ &= 2 + 57.58 \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4}\end{aligned}$$

$$\Rightarrow h = \frac{k}{d} Nu$$

$$= \frac{0.0411}{0.05} \times \left[ 2 + 57.58 \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \right]$$

$$= 1.644 + 47.33 \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4}$$

Now, Heat transfer rate between sphere and  $8^{\circ}\text{C}$   
is given as  $\dot{Q} = 7 \text{ W}$

$$\Rightarrow \dot{Q} = 7 \text{ W} = h A_s (T_s - T_{\infty})$$

$T_s$  = surface temperature of steel sphere

$$\Rightarrow 7 = h (4\pi r^2) (T_s - T_{\infty})$$

$$\Rightarrow 7 = h (4\pi (\frac{0.05}{2})^2) (T_s - T_{\infty})$$

$$\Rightarrow 890.9 = h (T_s - T_{\infty})$$

$$\Rightarrow 890.9 = \left[ 1.644 + 47.33 \left( \frac{\mu_{\infty}}{\mu_s} \right)^{1/4} \right] (T_s - 340) \quad ①$$

Now, dynamic viscosities of gas at different temperatures  
are given by

$$\mu_{\infty} = \mu_{340\text{K}} = 2.833 \times 10^{-5}$$

$$\mu_s = \mu_{0\text{K}}$$

$$\mu_{320\text{K}} = 2.758 \times 10^{-5}$$

$\Rightarrow$  By interpolation  $\rightarrow$

$$\mu_T = (1.545 - 0.0038T) \times 10^{-5}$$

Putting in equation ① →

$$890.9 = \left[ 1.644 + 47.33 \times \left( \frac{2.833}{1.545 - 0.0038T_s} \right)^{1/4} \right] (T_s - 340)$$

By solving above equation, we get

$$\boxed{T_s = 349.7 \text{ K}}$$

surface temperature of sphere